



Overturn study in the moon thermal evolution

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Overview

- Moon formation : giant impact between Earth and a Mars-sized body
- fully molten moon
- cooling and solidification in two steps
 - ▶ *radiative cooling with olivine-pyroxene cumulates*
 - ▶ *formation of anorthite crust (diffusion cooling)*

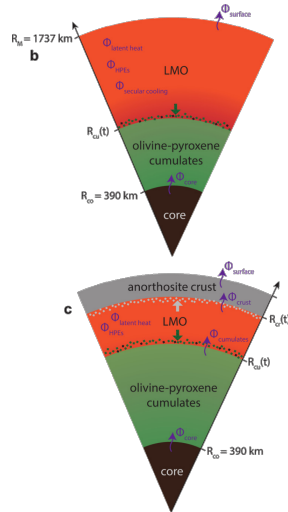


Figure – Moon formation

Radiative cooling

- Consider only a mix of anorthite and olivine-pyroxene

$$T_{\text{liq}} = T_{\text{OL}} - mC(t), \quad T_{\text{LMO}} = T_{\text{liq}}$$

- The conservation of anorthite yields :

$$(R_M^2 - R_{\text{co}}^2)C_0 = (R_M^3 - R_{\text{cu}}^3)C(t)$$

- We end up with the following :

$$T_{\text{liq}}(t) = T_{\text{OL}} - mC_0 \frac{R_M^3 - R_{\text{co}}^3}{R_M^3 - R_{\text{cu}}^3}$$

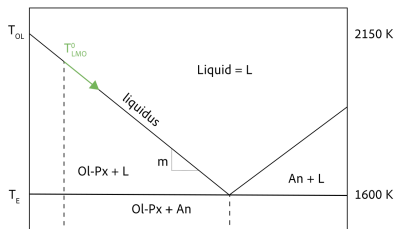


Figure – Phase diagram Olivine-pyrox / Anorthite

Radiative cooling

- Assuming that $T_{\text{cu}(r)} = T_{\text{liq}}(R_{\text{cu}}(t) = r)$ due to the short time scale of the first stage (neglect diffusion in the cumulate)
 - ▶ $10^2 \sim 10^3 \text{yr}$
 - ▶ *instable temperature profile*
- When $C(t) = C_E$ the anorthite crust is formed and slow down the cooling
- The cristallisation of the olivine is then slowed down (we can consider a constant width cumulates layer)
- However, this is instable density profile

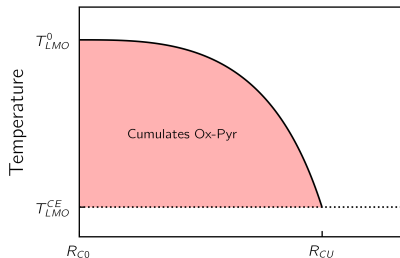


Figure – Instable temperature profile leading to overturn and increasing in flux

Modeling of the system

- We are interested in the dynamic of this cumulate layer at the beginning of the second stage
- The flux will increase and the temperature profile will be stable
- Convection in the 2d slab **Boussinesq** approximation with free slip boundary layer

$$\begin{cases} \vec{\nabla} \cdot \vec{u} = 0 \\ \rho_0 \frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \vec{\nabla} \vec{u} = \vec{\nabla} P + \eta \nabla^2 \vec{u} + \rho \vec{g} \\ \frac{\partial T}{\partial t} + \vec{u} \cdot \vec{\nabla} T = \kappa \nabla^2 T \\ \rho = \rho_0 (1 - \alpha (T - T_0)) \end{cases}$$

We expect to have thermal conduction driven Rayleigh-Bénard convection. This will lead to the following rescaling, filtering out the short time-scales:

$$\hat{x}, \hat{y} = \frac{\hat{x}}{d}, \frac{\hat{y}}{d} \quad \hat{z} = \frac{z}{d} + \frac{1}{2} \quad \hat{\theta} = \frac{\theta}{\Delta T_0} \quad \hat{t} = \frac{t \kappa}{d^2} \quad \hat{p} = \frac{p d^2}{\kappa \eta}$$

Modeling of the system

- We end up with the following dimensionless equations dropping the hats and considering infinite Prandtl number :

$$\begin{cases} \vec{\nabla} \cdot \vec{u} = 0 \\ \frac{1}{Pr} \frac{Du}{Dt} = -\vec{\nabla} p + \nabla^2 \vec{u} + Ra\theta \vec{e}_z = 0 \\ \frac{D\theta}{Dt} = \nabla^2 \theta \end{cases}$$

With $Ra = \frac{\rho_0 g \alpha \Delta T d^3}{\kappa \eta}$ and $Pr = \frac{\eta}{\kappa \rho_0}$. The infinite Prandtl approximation leads to a momentum dissipation greater than the thermal dissipation, the velocity field will then react immediately to a change of temperatures.

- The following boundary conditions are considered :
 - ▶ $\vec{u} \cdot \vec{e}_z = 0$ on $z = 0, 1$ (*impermeability*)
 - ▶ $\frac{\partial \theta}{\partial z} = 0$ on $z = 0$ (*negligible flux induced by the core*)
 - ▶ $\tau^x = 0$ on $z = 0, 1$ (*Free-slip*)
 - ▶ $\theta = 0$ on $z = 1$ (*Constant Temperature of the LMO*)



Motivation

- The goal of this project is to study the evolution of the cumulate layer at the beginning of the second stage of the moon cooling depending on the **temperature profiles** and on the range of **Ra**
- Study of the depth of the temperature profile and its impact on the thermal flux
- The moon cumulates Ra should be in the range $10^5 \sim 10^6$
 - ▶ *impact on the dynamics*
 - ▶ *this overturn flux is usually taken as : $\Phi_{OV} \sim e^{-\frac{t}{\tau_{OV}}}$*
 - ▶ *study this scaling law*



Numerical Setup

- Semi spectral method for convection-diffusion equations
- Fourier basis for the x basis (Periodic Boundary conditions)
- Chebyshev basis for the z basis (Allowing non-periodic boundary conditions)
- CGL nodes for the Chebyshev basis and equally spaced nodes for the Fourier basis
- Time integration using a second order Runge kutta scheme with adaptive time stepping



Initial Thermal conditions

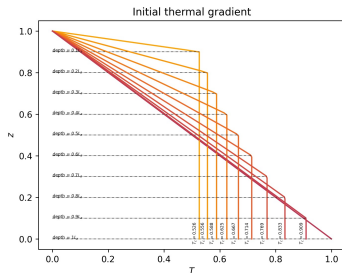


Figure – Initial temperature profile

- we ensure that the integral over all the depth is constant for all profile ensuring a constant amount of energy among all the profiles

$$T(z > e) = T_e + \frac{1 - z}{e(2 - e)}$$

Average temperature - Nusselt & Reynolds

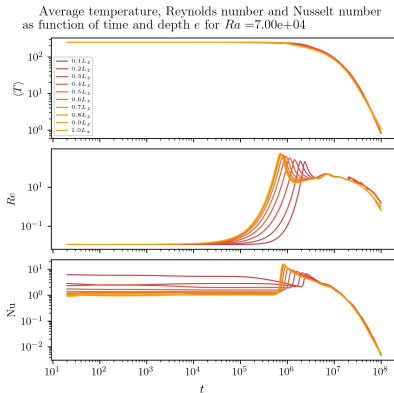


Figure – Average temperature profile
 Nusselt and Reynolds number for
 $Ra = 7.10^4$

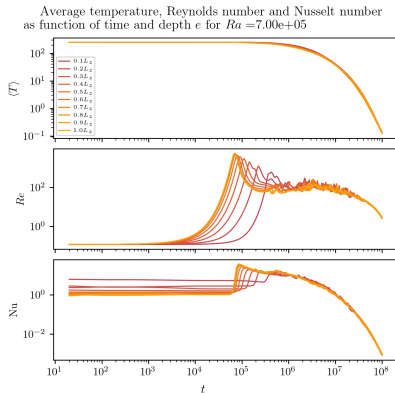
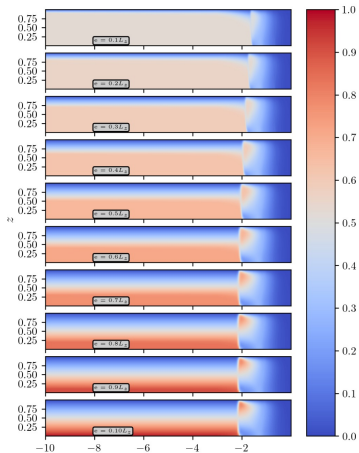


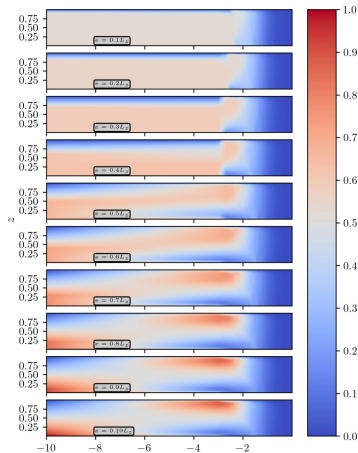
Figure – Average temperature profile
 Nusselt and Reynolds number for
 $Ra = 7.10^5$

Average temperature - Nusselt & Reynolds

Horizontally averaged temperature for all gradient
with $Ra = 7.00e+04$

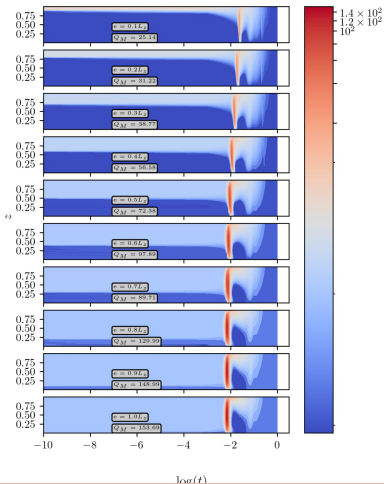


Horizontally averaged temperature for all gradient
with $Ra = 7.00e+05$

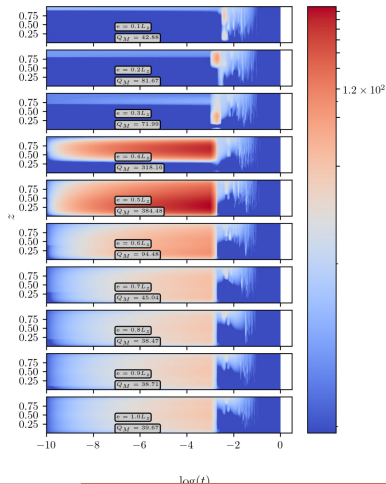


Overturn-Flux profile

Horizontally averaged heat flux for all gradient
with $Ra = 7.00e+04$



Horizontally averaged heat flux for all gradient
with $Ra = 7.00e+05$



Overturb-Flux profile

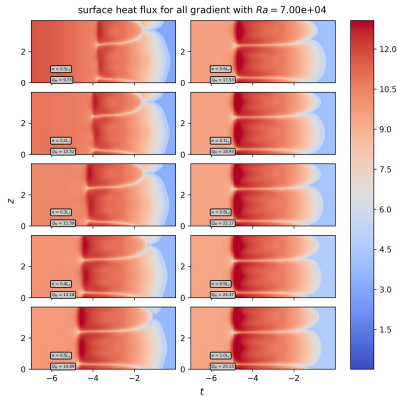


Figure – Surface heat flux for $Ra = 7.10^4$

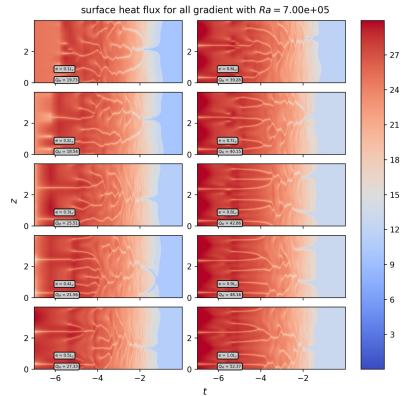
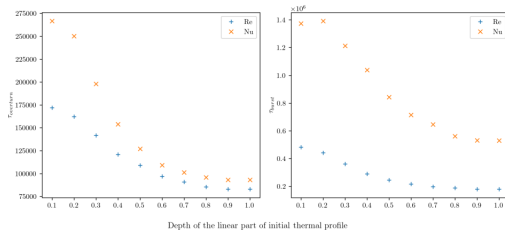
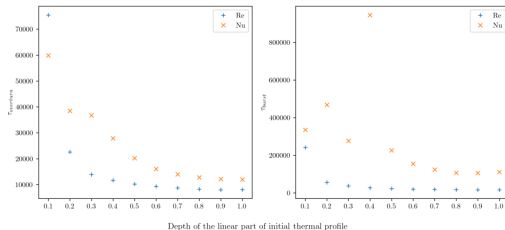


Figure – Surface heat flux for $Ra = 7.10^5$

Overturn and burst duration

Evolution of overturn time and release time for different initial thermal profile with $Ra = 7.00e+04$ Evolution of overturn time and release time for different initial thermal profile with $Ra = 7.00e+05$ 



Overturn and burst duration

Evolution of overturn date
for different initial thermal profil with $Ra = 7.00e+04$

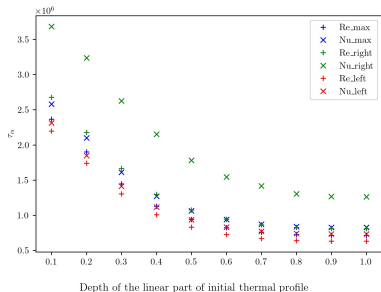


Figure – Overturn time for $Ra = 7.10^4$

Evolution of overturn date
for different initial thermal profil with $Ra = 7.00e+05$

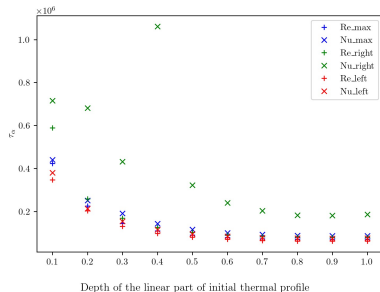


Figure – Overturn time for $Ra = 7.10^5$

Maximum Heat flux density in cumulates

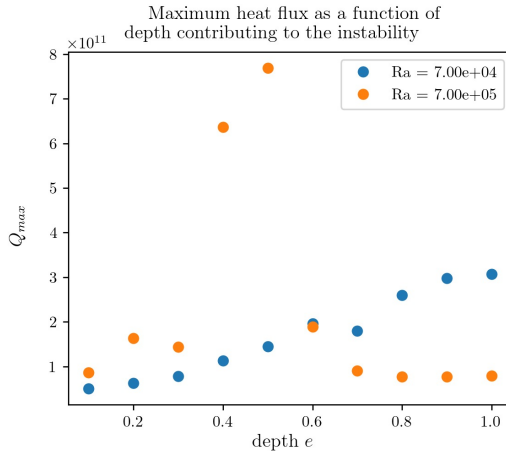
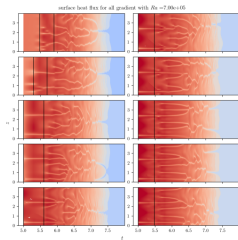
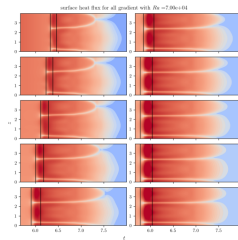
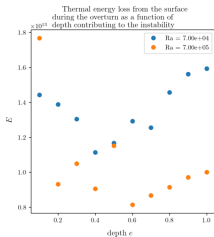


Figure – Maximum heat flux contribution for $Ra = 7 \cdot 10^4$ and $7 \cdot 10^5$

Loss of energy



Overturn and Burst duration

- Since the the overturn time and duration should be dependant of the convective time, the overturn time is dependant of the Rayleigh.
- More precisely, we expect the following scaling law :

$$\tau_{OV} \sim \tau_{conv} = Ra^{-1} \tau_{diffusion}$$

- For this we can study the total flux : $\Phi_{tot}(z=0) = V\theta - \partial_z\theta$

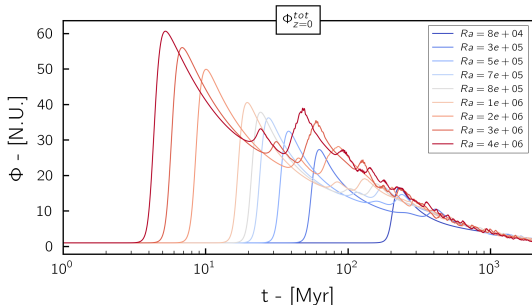


Figure – Overturn Dynamics for different Ra.

Overturn and Burst duration

The overturn time and the duration of the overturn dependency are plotted bellows :

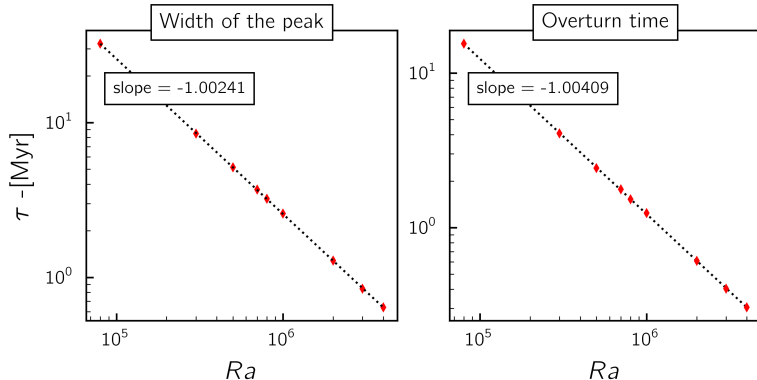


Figure – The overturn characteristic times are only convective scaling like predicted as Ra^{-1} , a diffusive behavior would have led to a scaling like Ra^1

Overturn and Burst duration

- One could suggest to rescale the time using the Rayleigh number to have comparable dynamics

$$\hat{t} = Ra \cdot t$$

- This unearthes very close dynamics for the different Rayleighs which seems to play a role only on the intensity of the convection events.

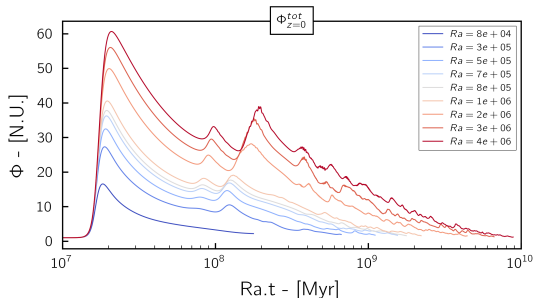


Figure – Rescaled overturn dynamics for different Ra.



Nusselt and Total Heat flux

- Next, we have to study the impact of the Ra on the intensity of the dynamics
- for large Rayleigh with overturn free dynamics one could unearth that the adimensional flux Nu verifies : $Nu \sim Ra^{\frac{1}{3}}$
- The nusselt number can be expressed as the ratio of the total flux and the conductive flux

$$Nu = \frac{\Phi_{\text{tot}}}{\Phi_{\text{cond}}} = \frac{V\theta - \partial_z \Theta}{\partial_z \Theta}$$

- in our study we have at $z = 0$, $v = 0$, we deduce easily that $Nu = 1$, and that the flux is only diffusive at the boundary. The study of the total flux will then be much more interesting.



Nusselt and Total Heat flux

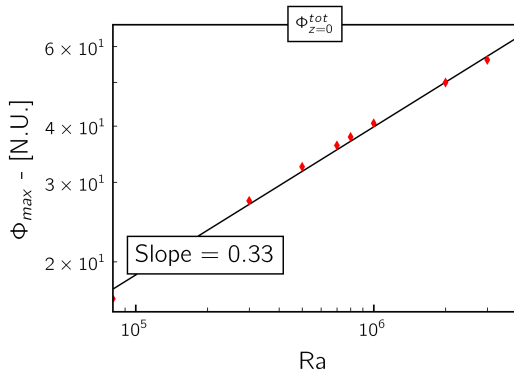


Figure – Φ^{max} scaling over the Raynold. We recover the previous law $Nu = Ra^{\frac{1}{3}}$



Modal analysis

- One could also study the convection events we saw before with multiple overturns occurring.
- For that we have to recall the first instable modes has a wavevector of value :
 - ▶ $k = 2.23$ for the free-free Boundary conditions
 - ▶ $k = 3.12$ for the rigid-rigid Boundary conditions (even modes)

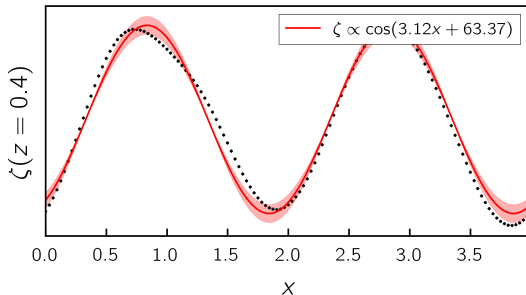
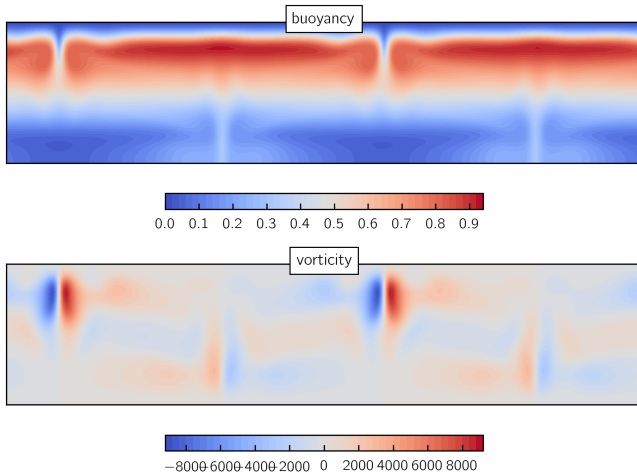


Figure – Vorticity profile before the first overturn, it seems that the BC are rigid (Pr infinite and $\theta(z=0) = 0$)

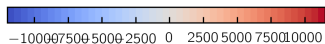
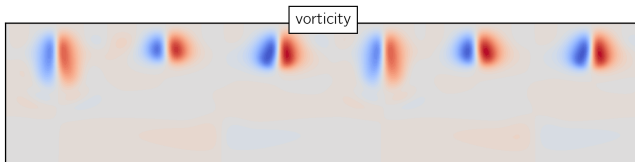
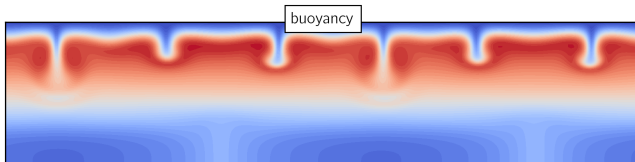
Modal analysis

Fields after the first overturn



Modal analysis

Fields just before the second overturn



Modal analysis

- All the natural frequencies of the system are then multiples of the first unstable mode, implying a cascade of convective cell fusion or division at different scales (This explains the characteristic cooling of the system that is not exponential).

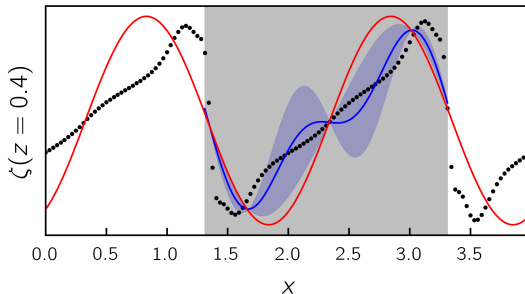


Figure – Vorticity profile after the first overturn, the BC are still rigid

Cooling rate

- The cooling is localized in a boundary layer at the top of the Box where the buoyancy is equilibrated by the diffusion processes.

$$\delta_T = \frac{L}{Ra^{\frac{1}{3}}}$$

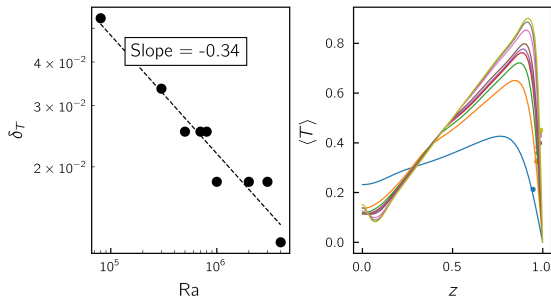


Figure – Temperature profile and boundary layer



Cooling rate

- Still have to determine the decaying scaling